

TWO INTERFACIAL COLLINEAR GRIFFITH CRACKS IN THERMO-ELASTIC COMPOSITE MEDIA

by

Prashant Kumar MISHRA and Subir DAS*

Department of Mathematical Sciences, Indian Institute of Technology, Varanasi, India

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The objective of the article is to find the stress intensity factors and crack energy for a pair of collinear Griffith cracks situated at the interface of the two orthotropic materials under steady-state temperature field. The problem is reduced to a pair of singular integral equations, which are solved using Jacobi's polynomials. Numerical computations are carried out for two different pairs of orthotropic materials for different particular cases, which are depicted through figures. The effect of material constants and temperature coefficients on the behavior of physical quantities viz., stress intensity factors and crack energy of the interfacial cracks is the key feature of the present article.

Key words: thermal stresses, collinear Griffith cracks, strain energy release rate, heat flux

Introduction

In many engineering disciplines viz., electronics, aerospace, and nuclear energy, lot of research has already been done during the study of behavior of the stress and displacement fields at the vicinity of the crack tip situated at the interface of the composite materials subject to thermal loading. Orthotropic composite materials are widely used in structural materials due to their light weight and strong in nature. When a cracked orthotropic composite material is used in a high or low temperature region, then heat flows through material. In this case, it is important to determine the thermal stress intensity around the crack, which occurs due to the disturbance in the heat flux. The investigation of thermo-elastic field and thermal stress concentration around the crack help to understand the stability and life of the cracked engineering materials and structures. According to linear elastic fracture mechanics, stress at the vicinity of the crack tip is singular. It is directly proportional to the inverse of square root of distance from the crack tip. Many observations of thermo-elastic cracked surfaces show that the thermal stress singularity at the vicinity of the crack tips are same as those with mechanical stresses. However, the nature of singularity becomes different for an interfacial crack. The occurrence of the interfacial cracks at the surface of structural components, due to thermal and mechanical loading, became an important research topic in fracture mechanics. For analyzing interfacial cracks, many studies were conducted under thermal steady-state conditions for orthotropic composite materials.

Sih [1] determined the stress intensity factor (SIF) of a crack in an infinite plate when the heat flows perpendicular to the crack surface. Later, Sekine [2] determined the SIF of a crack due to heat flux. The thermal stresses in an infinite plate due to the heat flux, for two

* Corresponding author, e-mail: sdas.apm@itbhu.ac.in

cracks have been determined by the same author [3]. The SIF around the two collinear cracks were evaluated by Chen and Zhang [4] in an orthotropic plate under the heat flux. Thermal stress for a single crack in an infinite elastic layer and thermal stress around two parallel cracks had been determined by Itou and Rengen [5]. Chen and Zhang [6] have determined the thermal stress in an orthotropic strip containing two collinear cracks. Itou [7] evaluated SIF for two parallel cracks in an infinite orthotropic plate due to the heat flux. Bakshi *et al.* [8] have solved the problem of determining the thermal stresses and displacement fields in an orthotropic plane containing a pair of equal collinear Griffith cracks using the integral transform technique based upon displacement potential under steady-state temperature field. Zhong *et al.* [9] examined the behavior of two collinear cracks embedded in an orthotropic solid, using the Fourier integral transform technique, under uniform heat flux and mechanical loading on the cracked surfaces. Problems related to thermal stress and strain can also be found in the research articles [10-15].

In the present article the authors have made an endeavor to determine the SIF at the tips of a pair of collinear Griffith cracks situated at the interface of two orthotropic thermo-elastic half planes subjected to a uniform heat flux and also to determine the energy required for creating two new surfaces and plastic deformation of the cracks under the steady-state temperature field. The problem has been reduced to a pair of second kind Fredholm integral equations, which are solved numerically using Jacobi polynomials. Numerical values of the SIF at the tips of the cracks for different prescribed crack lengths are presented through graphs for different particular cases. Numerical values of other physical quantity crack energy, obtained through different forms of the displacement potential functions, are also presented graphically.

Problem formulation

Let us consider a mathematical model of two bonded homogeneous orthotropic elastic half planes, $0 \leq y < \infty$ and $-\infty < y \leq 0$, containing a pair of collinear Griffith cracks situated symmetrically at the interface $y = 0$, when Cartesian co-ordinate axes coincide with the axes of symmetry of the elastic material. When thermal conditions are applied to the surface of an arbitrary 2-D orthotropic half planes, then the temperature field only depends on in-plane co-ordinates under the steady-state condition. The temperature distribution functions $T^{(i)}(x, y)$ are assumed to satisfy the following heat conduction equation in the orthotropic media.

$$\frac{\partial^2 T^{(i)}}{\partial x^2} + K^{(i)^2} \frac{\partial^2 T^{(i)}}{\partial y^2} = 0 \quad (1)$$

where $(K^{(i)})^2 = K_y^{(i)} / K_x^{(i)}$ and $K_y^{(i)}$ and $K_x^{(i)}$ ($i = 1, 2$) are the thermal conductive coefficients along y- and x-directions, respectively, for each half plane.

The general solution of $T^{(i)}(x, y)$ is (c. f., Clements and Tauchert [16]):

$$T^{(j)}(x, y) = \frac{1}{2\pi} \int_0^\infty \{A^{(j)}(p) e^{[p(ix-y/K^{(j)})]} + \bar{A}^{(j)}(p) e^{[p(-ix-y/K^{(j)})]}\} dp, \quad (2)$$

where $i = (-1)^{j/2}$, $j = 1, 2$ and $A^{(j)}(p)$ and $\bar{A}^{(j)}(p)$ are the arbitrary functions of p .

Here we have assumed that

$$T^{(i)}(x, 0) = h^{(i)}(x) \quad (3)$$

and hence the Fourier integral form of temperature distribution may be written:

$$T^{(i)}(x, 0) = \frac{1}{2\pi} \int_0^\infty \left\{ \int_{-\infty}^\infty h^{(i)}(\xi) e^{[p(i\xi)]} e^{[p(ix)]} + h^{(i)}(\xi) e^{[p(i\xi)]} e^{[p(-ix)]} d\xi \right\} dp \quad (4)$$

From eqs. (2) and (4), we get:

$$A^{(i)}(p) = \int_{-\infty}^{\infty} h^{(i)}(\xi) e^{-ip\xi} d\xi, \quad \bar{A}^{(i)}(p) = \int_{-\infty}^{\infty} h^{(i)}(\xi) e^{ip\xi} d\xi \quad (5)$$

From eqs. (2) and (5), the temperature distribution $T^{(i)}(x, y)$ is obtained:

$$T^{(i)}(x, y) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{y / K^{(i)} h^{(i)}(\xi) d\xi}{(y / K^{(i)})^2 + (\xi - x)^2} \quad (6)$$

If we consider $h^{(i)}(x) = \delta(x)$ (7)

where $h^{(i)}(x)$ is the prescribed temperature distribution become line source along y-axis and $\delta(x)$ is the Dirac delta function, the resultant temperature distribution is obtained:

$$T^{(i)}(x, y) = \frac{1}{\pi} \frac{(y / K^{(i)})}{(y / K^{(i)})^2 + x^2} \quad (8)$$

The relations between the plane stress, induced by the distribution of temperature, and displacement components $u^{(i)}(x, y)$ and $v^{(i)}(x, y)$ along x- and y-directions are given by:

$$\sigma_{xx}^{(i)}(x, y) = C_{11}^{(i)} \frac{\partial u^{(i)}}{\partial x} + C_{12}^{(i)} \frac{\partial v^{(i)}}{\partial y} - \beta_x^{(i)} T^{(i)} \quad (9)$$

$$\sigma_{yy}^{(i)}(x, y) = C_{12}^{(i)} \frac{\partial u^{(i)}}{\partial x} + C_{22}^{(i)} \frac{\partial v^{(i)}}{\partial y} - \beta_y^{(i)} T^{(i)} \quad (10)$$

$$\sigma_{xy}^{(i)}(x, y) = C_{66}^{(i)} \left(\frac{\partial u^{(i)}}{\partial x} + \frac{\partial v^{(i)}}{\partial y} \right) \quad (11)$$

where $C_{jk}^{(i)}$ are the elastic constants, $\beta_x^{(i)}$ and $\beta_y^{(i)}$ are the stress temperature coefficients. The displacement equations of equilibrium are given by:

$$C_{11}^{(i)} \frac{\partial^2 u^{(i)}}{\partial x^2} + C_{66}^{(i)} \frac{\partial^2 u^{(i)}}{\partial y^2} + [C_{12}^{(i)} + C_{66}^{(i)}] \frac{\partial^2 v^{(i)}}{\partial x \partial y} = \beta_x^{(i)} \frac{\partial T^{(i)}}{\partial x} \quad (12)$$

$$C_{22}^{(i)} \frac{\partial^2 v^{(i)}}{\partial y^2} + C_{66}^{(i)} \frac{\partial^2 v^{(i)}}{\partial x^2} + [C_{12}^{(i)} + C_{66}^{(i)}] \frac{\partial^2 u^{(i)}}{\partial x \partial y} = \beta_y^{(i)} \frac{\partial T^{(i)}}{\partial y} \quad (13)$$

The quantities with superscripts $i = 1, 2$ refer to those for the half plane-(1) and half plane-(2), respectively. It is assumed that at the interface $y = 0$, the cracks defined by $a < |x| < b$ are opened by internal normal and shearing tractions $p_1(x)$ and $p_2(x)$, respectively, fig. 1. For the described problem the boundary conditions on $y = 0$ are given by:

$$\sigma_{yy}^{(1)}(x, 0) = -p_1(x), \quad a \leq |x| \leq b \quad (14)$$

$$\sigma_{xy}^{(1)}(x, 0) = -p_2(x), \quad a \leq |x| \leq b \quad (15)$$

$$u^{(1)}(x, 0) = u^{(2)}(x, 0), \quad |x| < a, \quad |x| > b \quad (16)$$

$$v^{(1)}(x, 0) = v^{(2)}(x, 0), \quad |x| < a, \quad |x| > b \quad (17)$$

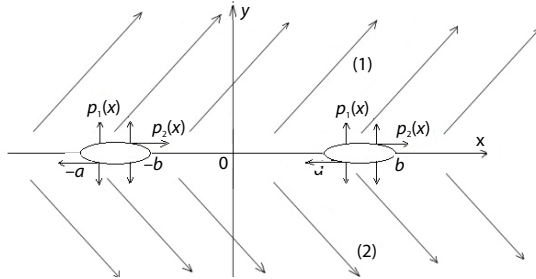


Figure 1. Geometry of the problem

$$\sigma_{yy}^{(1)}(x, 0) = \sigma_{yy}^{(2)}(x, 0), \quad -\infty < x < \infty \quad (18)$$

$$\sigma_{xy}^{(1)}(x, 0) = \sigma_{xy}^{(2)}(x, 0), \quad -\infty < x < \infty \quad (19)$$

Solution of the problem

During the solution of the problem, we first introduce displacement potentials $\psi^{(i)}(x, y)$ and $\phi_j^{(i)}(x, y)$ as, Sharma [17]:

$$\psi^{(i)}(x, y) = \frac{1}{2\pi} \int_0^\infty \{A^{(i)}(p)B^{(i)}(p)e^{p\{ix-(y/K)\}} + \bar{A}^{(i)}(p)\bar{B}^{(i)}(p)e^{p\{-ix-(y/K)\}}\} dp \quad (20)$$

Potential functions for the half planes are given by:

$$\phi_1^{(i)}(x, y) = \frac{2}{\pi} \int_0^\infty s^{-2} A_1^{(i)}(s) e^{-\frac{sy}{\sqrt{\mu_1^{(i)}}}} \cos(sx) ds \quad (21)$$

$$\phi_2^{(i)}(x, y) = \frac{2}{\pi} \int_0^\infty s^{-2} A_2^{(i)}(s) e^{-\frac{sy}{\sqrt{\mu_2^{(i)}}}} \cos(sx) ds, \quad i=1, 2 \quad (22)$$

The displacement components $u^{(i)}$ and $v^{(i)}$ are written:

$$u^{(i)} = \frac{\partial \psi^{(i)}}{\partial x} + \frac{\partial \phi_1^{(i)}}{\partial x} + \frac{\partial \phi_2^{(i)}}{\partial x} \quad \text{and} \quad v^{(i)} = \mu_1^{(i)} \frac{\partial \psi^{(i)}}{\partial y} + k_1^{(i)} \frac{\partial \phi_1^{(i)}}{\partial y} + k_2^{(i)} \frac{\partial \phi_2^{(i)}}{\partial y} \quad (23)$$

The corresponding thermal stresses are:

$$\frac{\sigma_{xx}^{(i)}(x, y)}{C_{66}^{(i)}} = - \left[(1+k_1^{(i)}) \frac{\partial^2 \phi_1^{(i)}}{\partial y^2} + (1+k_2^{(i)}) \frac{\partial^2 \phi_2^{(i)}}{\partial y^2} + (1+\eta^{(i)}) \frac{\partial^2 \psi^{(i)}}{\partial y^2} \right] \quad (24)$$

$$\frac{\sigma_{yy}^{(i)}(x, y)}{C_{66}^{(i)}} = \left[(1+k_1^{(i)}) \mu_1^{(i)} \frac{\partial^2 \phi_1^{(i)}}{\partial y^2} + (1+k_2^{(i)}) \mu_2^{(i)} \frac{\partial^2 \phi_2^{(i)}}{\partial y^2} - (1+\eta^{(i)}) \frac{\partial^2 \psi^{(i)}}{\partial x^2} \right] \quad (25)$$

$$\frac{\sigma_{xy}^{(i)}(x, y)}{C_{66}^{(i)}} = \left[(1+k_1^{(i)}) \frac{\partial^2 \phi_1^{(i)}}{\partial x \partial y} + (1+k_2^{(i)}) \frac{\partial^2 \phi_2^{(i)}}{\partial x \partial y} + (1+\eta^{(i)}) \frac{\partial^2 \psi^{(i)}}{\partial x \partial y} \right] \quad (26)$$

The displacement eqs. (12) and (13) are satisfied by eq. (20) for non-trivial $\phi_j^{(i)}$ if:

$$\eta^{(i)} = \frac{\beta_y^{(i)} [C_{66}^{(i)} - K^{(i)2} C_{11}^{(i)}] + \beta_x^{(i)} [C_{12}^{(i)} + C_{66}^{(i)}] K^{(i)2}}{\beta_x^{(i)} [C_{22}^{(i)} - K^{(i)2} C_{66}^{(i)}] - \beta_y^{(i)} [C_{12}^{(i)} + C_{66}^{(i)}]} \quad (27)$$

$$p^2 B = p^2 \bar{B} = K^{(i)2} \frac{\beta_x^{(i)} [C_{22}^{(i)} - K^{(i)2} C_{66}^{(i)}] - \beta_y^{(i)} [C_{12}^{(i)} + C_{66}^{(i)}]}{[C_{22}^{(i)} - K^{(i)2} C_{66}^{(i)}][C_{66}^{(i)} - K^{(i)2} C_{11}^{(i)}] + K^{(i)} [C_{12}^{(i)} + C_{66}^{(i)}]^2} = k \quad (28)$$

Here, the potential functions $\phi_j^{(i)}$ satisfies the following differential equations:

$$\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \phi_j^{(i)}(x, y) = 0, \quad i=1, 2, \quad j=1, 2$$

where $\mu_1^{(i)}$ and $\mu_2^{(i)}$ are the real roots of the equation:

$$C_{11}^{(i)} C_{66}^{(i)} \mu^{(i)2} + [(C_{12}^{(i)})^2 + 2C_{12}^{(i)} C_{66}^{(i)} - C_{11}^{(i)} C_{22}^{(i)}] \mu^{(i)} + C_{212}^{(i)} C_{66}^{(i)} = 0 \quad (29)$$

with

$$k_j^{(i)} = \frac{C_{11}^{(i)} \mu_j^{(i)} - C_{66}^{(i)}}{C_{66}^{(i)} + C_{12}^{(i)}} \quad (30)$$

$A_1^{(i)}(s)$ and $A_2^{(i)}(s)$ ($i = 1, 2$) are the undetermined functions. Applying the boundary conditions (18) and (19), we get:

$$A_1^{(2)}(s) = \frac{k^{(2)}(1+\eta^{(2)})\sqrt{\mu_1^{(2)}}}{2(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}})(1+k_1^{(2)})} \left(\frac{K^{(2)} - \sqrt{\mu_2^{(2)}}}{K^{(2)}} \right) + \frac{C_{66}^{(1)}}{C_{66}^{(2)}} \frac{k^{(1)}(1+\eta^{(1)})}{2K^{(1)}} \frac{\sqrt{\mu_1^{(2)}}(\sqrt{\mu_{22}^{(2)}} - K^{(1)})}{(1+k_1^{(2)})(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}})} +$$

$$+ A_1^{(1)}(s) \frac{\sqrt{\mu_1^{(2)}}(1+k_1^{(1)})(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(1)}})}{\sqrt{\mu_1^{(1)}}(1+k_1^{(2)})(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}})} + A_2^{(1)}(s) \frac{\sqrt{\mu_1^{(2)}}(1+k_2^{(1)})(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_2^{(1)}})}{\sqrt{\mu_2^{(1)}}(1+k_1^{(2)})(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}})}$$

$$A_2^{(2)}(s) = \frac{k^{(2)}(1+\eta^{(2)})\sqrt{\mu_2^{(2)}}}{2(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}})(1+k_2^{(2)})} \left(\frac{K^{(2)} - \sqrt{\mu_1^{(2)}}}{K^{(2)}} \right) + \frac{C_{66}^{(1)}}{C_{66}^{(2)}} \frac{k^{(1)}(1+\eta^{(1)})}{2K^{(1)}} \frac{\sqrt{\mu_2^{(2)}}(\sqrt{\mu_{21}^{(2)}} - K^{(1)})}{(1+k_2^{(2)})(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}})} +$$

$$+ A_1^{(1)}(s) \frac{\sqrt{\mu_2^{(2)}}(1+k_1^{(1)})(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_1^{(1)}})}{\sqrt{\mu_1^{(1)}}(1+k_2^{(2)})(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}})} + A_2^{(1)}(s) \frac{\sqrt{\mu_2^{(2)}}(1+k_2^{(1)})(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(1)}})}{\sqrt{\mu_2^{(1)}}(1+k_2^{(2)})(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}})}$$

Boundary conditions (16) and (17), with the help of the previous equations, give rise to:

$$\int_0^{\infty} \{ \alpha_1 + \alpha_2 A_1^{(1)}(s) + \alpha_3 A_2^{(1)}(s) \} \frac{\sin(sx)}{s} dx = 0, \quad 0 < x < a, \quad b < x < \infty$$

$$\int_0^{\infty} \{ \beta_1 + \beta_2 A_1^{(1)}(s) + \beta_3 A_2^{(1)}(s) \} \frac{\cos(sx)}{s} dx = 0, \quad 0 < x < a, \quad b < x < \infty$$

Now setting:

$$\alpha_1 + \alpha_2 A_1^{(1)}(s) + \alpha_3 A_2^{(1)}(s) = \int_a^b f_1(t) \cos(st) dt$$

$$\beta_1 + \beta_2 A_1^{(1)}(s) + \beta_3 A_2^{(1)}(s) = \int_a^b f_2(t) \sin(st) dt$$

where

$$\alpha_1 = \frac{k^{(1)} - k^{(2)}}{2} - \left[\frac{k^{(2)}(1+\eta^{(2)})\sqrt{\mu_1^{(2)}}}{2(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}})(1+k_1^{(2)})} \left(\frac{K^{(2)} - \sqrt{\mu_2^{(2)}}}{K^{(2)}} \right) + \frac{C_{66}^{(1)}}{C_{66}^{(2)}} \frac{k^{(1)}(1+\eta^{(1)})}{2K^{(1)}} \frac{\sqrt{\mu_1^{(2)}}(\sqrt{\mu_{22}^{(2)}} - K^{(1)})}{(1+k_1^{(2)})(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}})} \right] -$$

$$\left[\frac{k^{(2)}(1+\eta^{(2)})\sqrt{\mu_2^{(2)}}}{2(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}})(1+k_2^{(2)})} \left(\frac{K^{(2)} - \sqrt{\mu_1^{(2)}}}{K^{(2)}} \right) + \frac{C_{66}^{(1)}}{C_{66}^{(2)}} \frac{k^{(1)}(1+\eta^{(1)})}{2K^{(1)}} \frac{\sqrt{\mu_2^{(2)}}(\sqrt{\mu_{21}^{(2)}} - K^{(1)})}{(1+k_2^{(2)})(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}})} \right]$$

$$\alpha_2 = 1 - \frac{\sqrt{\mu_1^{(2)}}(1+k_1^{(1)})\left(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(1)}}\right)}{\sqrt{\mu_1^{(1)}}(1+k_1^{(2)})\left(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}}\right)} - \frac{\sqrt{\mu_2^{(2)}}(1+k_1^{(1)})\left(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_1^{(1)}}\right)}{\sqrt{\mu_1^{(1)}}(1+k_2^{(2)})\left(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}}\right)}$$

$$\alpha_3 = 1 - \frac{\sqrt{\mu_1^{(2)}}(1+k_2^{(1)})\left(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_2^{(1)}}\right)}{\sqrt{\mu_2^{(1)}}(1+k_1^{(2)})\left(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}}\right)} - \frac{\sqrt{\mu_2^{(2)}}(1+k_2^{(1)})\left(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(1)}}\right)}{\sqrt{\mu_2^{(1)}}(1+k_2^{(2)})\left(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}}\right)}$$

$$\beta_1 = \frac{k^{(1)}\eta^{(1)}}{2K^{(1)}} - \frac{k^{(2)}\eta^{(2)}}{2K^{(2)}}$$

$$\beta_2 = \frac{k_1^{(1)}}{\sqrt{\mu_1^{(1)}}} + \frac{k_1^{(2)}}{\sqrt{\mu_1^{(2)}}} \frac{\sqrt{\mu_1^{(2)}}(1+k_1^{(1)})\left(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(1)}}\right)}{\sqrt{\mu_1^{(1)}}(1+k_1^{(2)})\left(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}}\right)} + \frac{k_2^{(2)}}{\sqrt{\mu_2^{(2)}}} \frac{\sqrt{\mu_2^{(2)}}(1+k_1^{(1)})\left(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_1^{(1)}}\right)}{\sqrt{\mu_1^{(1)}}(1+k_2^{(2)})\left(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}}\right)}$$

$$\beta_3 = \frac{k_2^{(1)}}{\sqrt{\mu_2^{(1)}}} + \frac{k_1^{(2)}}{\sqrt{\mu_1^{(2)}}} \frac{\sqrt{\mu_1^{(2)}}(1+k_2^{(1)})\left(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_2^{(1)}}\right)}{\sqrt{\mu_2^{(1)}}(1+k_1^{(2)})\left(\sqrt{\mu_2^{(2)}} - \sqrt{\mu_1^{(2)}}\right)} + \frac{k_2^{(2)}}{\sqrt{\mu_2^{(2)}}} \frac{\sqrt{\mu_2^{(2)}}(1+k_2^{(1)})\left(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(1)}}\right)}{\sqrt{\mu_2^{(1)}}(1+k_2^{(2)})\left(\sqrt{\mu_1^{(2)}} - \sqrt{\mu_2^{(2)}}\right)}$$

and after lengthy process of mathematical manipulations, boundary conditions (14) and (15) finally lead to the following singular integral equations:

$$a_1 f_1(x) + \frac{2}{\pi} \int_a^b \frac{f_2(t)}{(t-x)} dt = -\frac{2}{\pi} p_1(x) \quad a \leq |x| \leq b \quad (31)$$

$$c_1 f_2(x) + \frac{2}{\pi d_1} \int_a^b \frac{f_1(t)}{(t-x)} dt = -\frac{2}{\pi} p_2(x) - \frac{2c}{\pi x} \quad a \leq |x| \leq b \quad (32)$$

where

$$a_1 = \frac{2}{\pi} C_{66}^{(1)} \left[(1+k_1^{(1)}) \left(\frac{\beta_3}{\beta_3 \alpha_2 - \alpha_3 \beta_2} \right) + (1+k_2^{(1)}) \left(\frac{\beta_2}{\beta_2 \alpha_3 - \alpha_2 \beta_3} \right) \right]$$

$$\frac{1}{b_1} = \frac{2}{\pi} C_{66}^{(1)} \left[(1+k_1^{(1)}) \left(\frac{\alpha_3}{\beta_3 \alpha_2 - \alpha_3 \beta_2} \right) + (1+k_2^{(1)}) \left(\frac{\alpha_2}{\beta_2 \alpha_3 - \alpha_2 \beta_3} \right) \right]$$

$$c_1 = \frac{2}{\pi} C_{66}^{(1)} \left[\frac{(1+k_1^{(1)})}{\sqrt{\mu_1^{(1)}}} \left(\frac{\alpha_3}{\beta_3 \alpha_2 - \alpha_3 \beta_2} \right) + \frac{(1+k_2^{(1)})}{\sqrt{\mu_2^{(1)}}} \left(\frac{\alpha_2}{\beta_2 \alpha_3 - \alpha_2 \beta_3} \right) \right]$$

$$\frac{1}{d_1} = \frac{2}{\pi} C_{66}^{(1)} \left[\frac{(1+k_1^{(1)})}{\sqrt{\mu_1^{(1)}}} \left(\frac{\beta_3}{\beta_3 \alpha_2 - \alpha_3 \beta_2} \right) + \frac{(1+k_2^{(1)})}{\sqrt{\mu_2^{(1)}}} \left(\frac{\beta_2}{\beta_2 \alpha_3 - \alpha_2 \beta_3} \right) \right]$$

$$c = \frac{(1+k_1^{(1)})}{\sqrt{\mu_1^{(1)}}} \left(\frac{\alpha_3 \beta_1 - \alpha_1 \beta_3}{\beta_3 \alpha_2 - \alpha_3 \beta_2} \right) + \frac{(1+k_2^{(1)})}{\sqrt{\mu_2^{(1)}}} \left(\frac{\alpha_2 \beta_1 - \alpha_1 \beta_2}{\beta_2 \alpha_3 - \alpha_2 \beta_3} \right) + \frac{(1+\eta^{(1)})}{2} \frac{k^{(1)}}{K^{(1)}} \quad (33)$$

Equations (31) and (32) are reduced to the following singular integral equations for the determination of unknown functions $f_i(x)$:

$$\phi_k(x) + \frac{1}{\pi i \varepsilon_k r_k} \int_a^b \frac{\phi_k(t)}{(t-x)} dt = -g_k(x) - \frac{2ic}{\pi r_k x} \quad a \leq |x| \leq b \quad (34)$$

where

$$\begin{aligned} \phi_k(x) &= \sqrt{a_1 b_1} f_1(x) + i r_k \sqrt{c_1 d_1} f_2(x), \quad k=1,2 \\ \varepsilon &= \sqrt{a_1 b_1 c_1 d_1}, \quad r_k = (-1)^{k+1}, \quad k=1,2 \\ g_k(x) &= \frac{2}{\pi} [\sqrt{b_1 / a_1} p_1(x) + r_k \sqrt{d_1 / c_1} p_2(x)] \quad k=1,2 \end{aligned}$$

and $f_i(x)$ are satisfying the conditions:

$$\int_a^b f_i(t) dt = 0, \quad i=1,2$$

The solution of the previous integral equations in (34) may be assumed:

$$\phi_k(x) = \omega_k(x) \sum_{n=0}^{\infty} c_{kn} P_n^{(\alpha_k, \beta_k)}(x), \quad k=1,2 \quad (35)$$

where $\omega_k(x) = (1-x)^{\alpha_k} (1+x)^{\beta_k}$

$$\alpha_k = -\frac{1}{2} + i\omega_k, \quad \beta_k = -\frac{1}{2} - i\omega_k, \quad \omega_k = r_k \omega \quad \text{and} \quad \frac{1}{2\pi} \ln \left| \frac{1}{1-x} \right|$$

with c_{kn} as unknown constants. Now, using eq. (33), we get:

$$\int_a^b \phi_i(t) dt = 0, \quad i=1,2$$

which implies $C_{k0} = 0, k=1, 2$.

From eqs. (31) and (32), we get:

$$\omega_k(x) \sum_{n=1}^{\infty} c_{kn} P_n^{(\alpha_k, \beta_k)}(x) + \frac{2}{\pi i \varepsilon_k r_k} \int_a^b \frac{\omega_k(t) \sum_{n=0}^{\infty} c_{kn} P_n^{(\alpha_k, \beta_k)}(t)}{(t-x)} dt = -g_k(x) - \frac{2ic}{\pi r_k} \sqrt{\frac{d_1}{c_1}} \frac{1}{x} \quad (36)$$

Multiplying the previous equation by $P_j^{(\alpha_k, \beta_k)}(x)$ and integrating from -1 to 1 , we get:

$$c_{kj} \theta_j^{(\alpha_k, \beta_k)} + \frac{2}{\pi i \varepsilon_k r_k} \sum_{n=1}^{\infty} c_{kn} L_{nj} = -F_{kj} - \frac{2ic}{\pi r_k} \sqrt{\frac{d_1}{c_1}} \int_{-1}^1 \frac{P_j^{(\alpha_k, \beta_k)}(x)}{x} dx \quad (37)$$

where

$$\theta_j^{(\alpha_k, \beta_k)} = \frac{2^{\alpha_k + \beta_k + 1}}{2j + \alpha_k + \beta_k + 1} \frac{\Gamma(j + \alpha_k + 1) \Gamma(j + \beta_k + 1)}{\Gamma(j + \alpha_k + \beta_k + 1) j!}$$

$$L_{nj} = \int_{-1}^1 P_j^{(\alpha_k, \beta_k)}(x) \int_a^b \frac{\omega_k(t) P_n^{(\alpha_k, \beta_k)}(t)}{(t-x)} dt dx \quad F_{kj} = \int g_k(x) P_j^{(\alpha_k, \beta_k)}(x) dx$$

and the principal value of $\int_{-1}^1 dx / x$ is considered as zero.

Finally, the stress intensity factors at the crack tips $x = a$ and $x = b$ are calculated:

$$\begin{aligned} \sqrt{b_1/a_1} K_I^a + ir_k \sqrt{d_1/c_1} K_{II}^a &= \lim_{x \rightarrow a^-} (x-a)^{-\alpha_k} (x+a)^{-\beta_k} [\sqrt{b_1/a_1} \sigma_{yy}^{(1)}(x,0) + ir_k \sqrt{d_1/c_1} \sigma_{xy}^{(1)}(x,0)] = \\ &= \frac{(-1)^{\alpha_k} \pi a}{2} \sum_{n=1}^{\infty} c_{kn} P_n^{(\alpha_k, \beta_k)}(1), \quad k=1,2 \end{aligned} \quad (38)$$

$$\begin{aligned} \sqrt{b_1/a_1} K_I^b + ir_k \sqrt{d_1/c_1} K_{II}^b &= \lim_{x \rightarrow b^+} (x-b)^{-\alpha_k} (x+b)^{-\beta_k} [\sqrt{b_1/a_1} \sigma_{yy}^{(1)}(x,0) + ir_k \sqrt{d_1/c_1} \sigma_{xy}^{(1)}(x,0)] = \\ &= \frac{(-1)^{\alpha_k} \pi b}{2} \sum_{n=1}^{\infty} c_{kn} P_n^{(\alpha_k, \beta_k)}(1), \quad k=1,2 \end{aligned} \quad (39)$$

The crack energy is calculated:

$$W = \int_a^b p_1(x) [v^{(1)}(x,0) - v^{(2)}(x,0)] dx \quad (40)$$

Results and discussion

In this section, the numerical computations have been done to find physical quantities viz., SIF and the crack energy for two collinear cracks situated at the interface of two pairs of orthotropic materials with first one as α -uranium and epoxy boron, and the second one as beryllium and epoxy boron. In each case first type of material is taken as half plane-1 and second type of material as half plane-2. During the computations the crack length is considered as $b=1$ and $a = 0.1$ (0.1) 0.9 and also the loadings are considered as $p_1(x) = p$, $p_2(x) = 0$. The ratios of the stress temperature coefficients $\beta_y^{(1)}/\beta_x^{(1)}$ and $\beta_y^{(2)}/\beta_x^{(2)}$ are taken as 0.67 and 0.5, respectively, for the first pair of materials, and 0.7 and 0.5, respectively, for second pair of materials. The elastic constants of the orthotropic material α -uranium have been taken as $C_{11} = 21.47 \cdot 10^6$ psi (148.03 GPa), $C_{12} = 4.65 \cdot 10^6$ psi (32.06 GPa), $C_{22} = 19.36 \cdot 10^6$ psi (133.48 GPa), $C_{66} = 7.43 \cdot 10^6$ psi (51.22 GPa), Das and Patra [18]. The elastic constants of the other considered orthotropic material boron-epoxy has been taken as $C_{11} = 30.3 \cdot 10^6$ psi (208.91 GPa), $C_{12} = 3.78 \cdot 10^6$ psi (26.06 GPa), $C_{22} = 4.04 \cdot 10^6$ psi (27.85 GPa), $C_{66} = 1.13 \cdot 10^6$ psi (7.79 GPa), (Sih and Chen [19]), and those of orthotropic material beryllium are taken as $C_{12} = 8.88 \cdot 10^6$ psi (61.22 GPa), $C_{22} = 36.49 \cdot 10^6$ psi (251.58 GPa), $C_{66} = 11.24 \cdot 10^6$ psi (77.4 GPa), Das and Patra [18]. For the first and second pair of materials, the SIF at the tip $x = a$ are described through fig. 2 and 3, respectively, for different values of a/b , whereas the physical quantities at the tip $x = b$ for both the pair of materials are depicted through figs. 4 and 5 for various a/b . The numerical values of crack energies for the two pairs of materials are shown through figs. 6 and 7 for different values of a/b .

It is seen from fig. 2 that as the length of the crack decreases, both K_I^a and K_{II}^a decrease. Same nature is followed for the second pair of materials, fig. 3, with only difference is that the values of SIF change as it completely depends on material constants.

As the lengths of the cracks decrease, figs. 4 and 5, i. e., cracks separation distance increases, then K_I^b decreases, K_{II}^b increases under thermo-mechanical loading for both pairs of materials. This shows that there is a least possibility of crack propagation at $x = b$, even when the tips of the cracks come very close to each other. The decreases of Mode II stress intensity factor justifies that as the distance between two cracks decreases, the effect of their propagation tendency in sliding mode will be decreased.

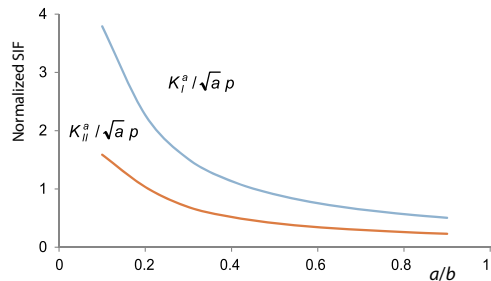


Figure 2. Plots of $K_I^a/a^{1/2}p$ and $K_{II}^a/a^{1/2}p$ vs. a/b for the first pair of materials

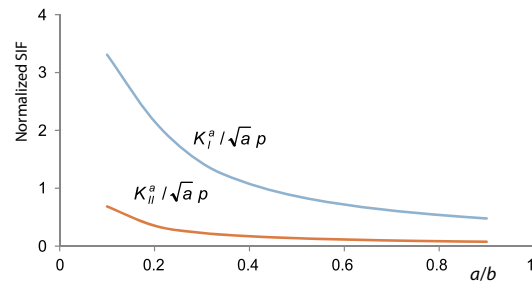


Figure 3. Plots of $K_I^a/a^{1/2}p$ and $K_{II}^a/a^{1/2}p$ vs. a/b for the second pair of materials

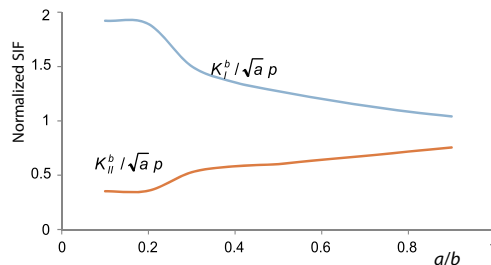


Figure 4. Plots of $K_I^b/a^{1/2}p$ and $K_{II}^b/a^{1/2}p$ vs. a/b for the first pair of materials

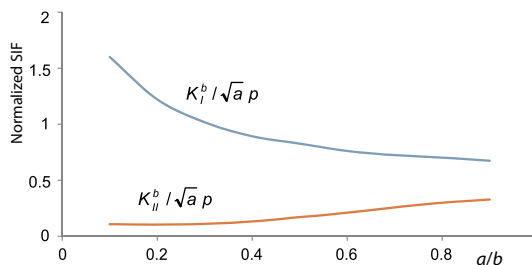


Figure 5. Plots of $K_I^b/a^{1/2}p$ and $K_{II}^b/a^{1/2}p$ vs. a/b for the second pair of materials

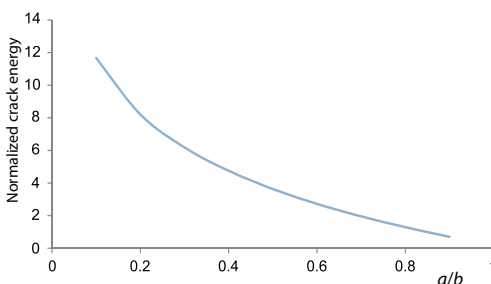


Figure 6. Plot of W/ap vs. a/b for the first pair of materials

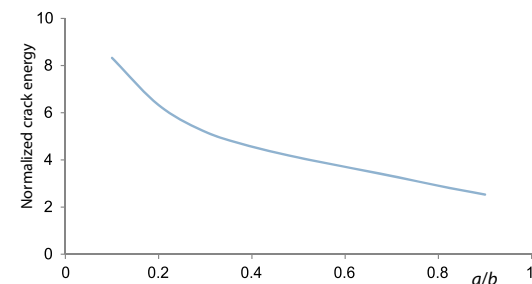


Figure 7. Plot of W/ap vs. a/b for the second pair of materials

The nature of behavior of crack energy for first pair of materials is same as the second pair of materials with the difference is that in first case the nature of the decrease is very fast as compared to the gradually decrease of the second case.

In the numerical computation it is also given special emphasis to determine other physical quantity crack energy, W , to determine the energy required by the crack per unit increase in area. Figures 6 and 7 show that the crack energy increases with the increase of crack length. The increment of crack energy represents that as crack advances then plastic zone size becomes large due to which more energy will be required for the crack propagation after attaining its critical value.

It is seen from the figs. 2-5 that first pair of materials can sustain more stress intensity compared to second pair of materials without fracture and it is also justified from figs. 6 and 7 that for the first pair of materials the crack energy is higher compared to the second pair of materials due to formation of large plastic zone at the crack tips with increase of crack length.

Conclusion

In the present article the authors have achieved four important goals. The first one is the investigation of a pair of collinear Griffith cracks at the interface of two orthotropic media under thermo mechanical loading. Second one is finding the analytical form of the stress intensity factors at the vicinity of the crack tips. Third one is the successful presentation of variations of the SIF with crack separation distance. Fourth one is the increase of crack energy due to increase of length of the cracks showing the possibility of the formation of large plastic zone at the vicinity of the crack tip.

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Nomenclature

a, b – boundary points of the crack, [m]
 $K_I^a/a^{1/2}p, K_I^b/a^{1/2}p$ – normalized SIF of Mode I type
 at $x = a$ and $x = b$, respectively, [–]
 $K_{II}^a/a^{1/2}p, K_{II}^b/a^{1/2}p$ – normalized SIF of Mode II
 type at $x = a$ and $x = b$, respectively, [–]
 K^0 – the ratio of thermal conductive coefficients along
 the y- and x-directions, respectively, [–]
 T^0 – temperature distribution function, [°C]

$u^{(i)}, v^{(i)}$ – displacement components, [m]
 W/ap – normalized crack energy, [–]

Greek symbols

$\beta_x^{(i)}, \beta_y^{(i)}$ – stress temperature coefficients, [GPa°C⁻¹]
 $\sigma_x^{(i)}, \sigma_y^{(i)}$ – stress tensors along the x and y axis,
 respectively, [GPa]
 $\sigma_{xy}^{(i)}$ – shear stress tensor, [GPa]

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